



# Theory of fiberoptic current sensors

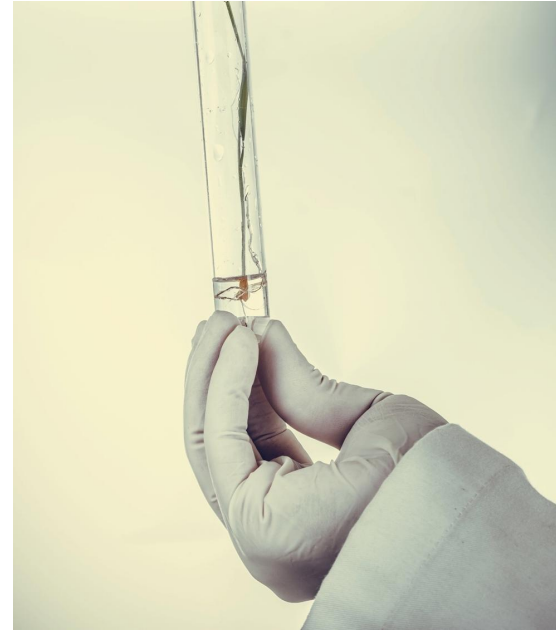
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19 April 2017

Research Institutes of Sweden

**Safety and Transport**

Measurement Science and Technology – Time and optics



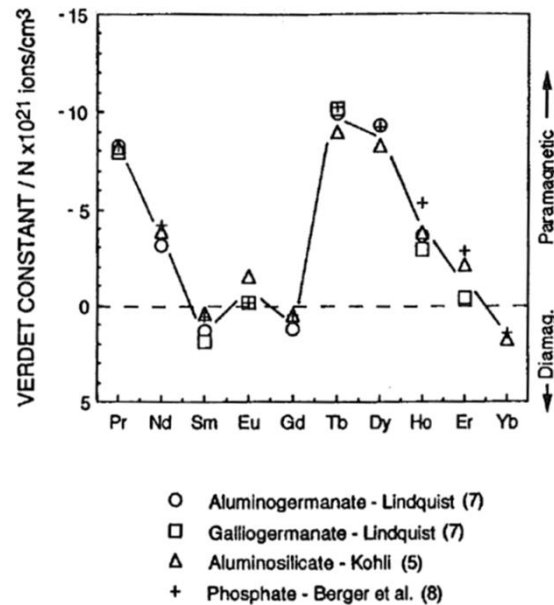


# Theory of fiberoptic current sensors

- Background – the Faraday effect
- Polarization measurement
- Interferometric methods
- Phase modulation
- FOCS setup
- Fiber properties

# Background – the Faraday effect

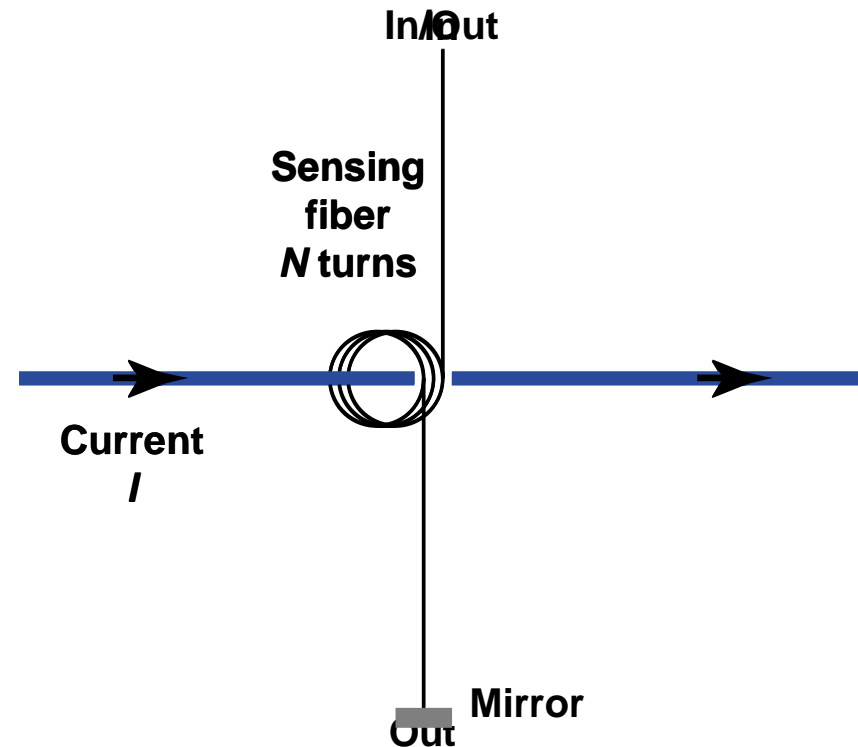
- Fibers are generally insensitive to disturbance
- Michael Faraday 1845: light is influenced by an external magnetic field
- Electro-optic modulator
- Nonreciprocal effect
- Verdet constant is material specific
- Doping with rare-earths may increase V



| Material                        | Verdet constant V<br>(10 <sup>3</sup> min of arc G <sup>-1</sup> cm <sup>-1</sup> ) | Wavelength<br>(nm) |
|---------------------------------|---|--------------------|
| H <sub>2</sub> O                | 13,11   | 500                |
|                                 | 12,6  | 600                |
|                                 | 7,0   | 800                |
|                                 | 4,4   | 1000               |
|                                 | 2,9   | 1250               |
| CCl <sub>4</sub>                | 16,03   | 600                |
|                                 | 8,9   | 800                |
|                                 | 5,7   | 1000               |
|                                 | 2,5   | 1500               |
|                                 | 1,3   | 2000               |
|                                 | C <sub>6</sub> H <sub>6</sub>   | 29,7               |
| 15,3                            |   | 800                |
| 9,5                             |   | 1000               |
| 3,9                             |   | 1500               |
| 2,2                             |   | 2000               |
| CS <sub>2</sub>                 |   | 43,41              |
|                                 | 21,4  | 800                |
|                                 | 13,5  | 1000               |
|                                 | 5,8   | 1500               |
|                                 | 3,1   | 2000               |
| ZnS                             | 225   |                    |
| NaCl                            | 35,85   |                    |
| KCl                             | 28,58   |                    |
| PbO SiO <sub>2</sub><br>(glass) | 77,9  |                    |
| Tb-doped<br>glass               | 213   | 1053               |

# Background – the Faraday effect

- Fiber coil instead
- $N$  number of turns in coil
- Ampere's law gives a closed line integral:  $\theta_f = \oint \mathbf{B} \cdot d\mathbf{l} = \mu_0 \oint N I$
- End mirror creates double passage



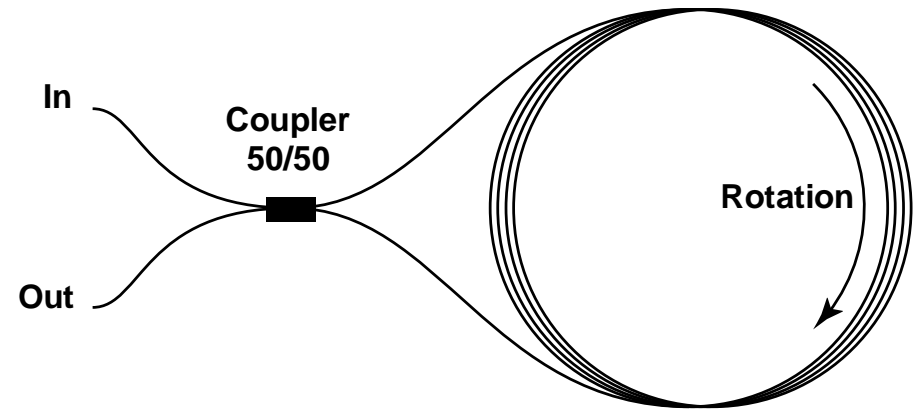
# Polarization measurement

- Direct measurement of polarization
- Accuracy and speed
- Difficult to measure 50-Hz and harmonics



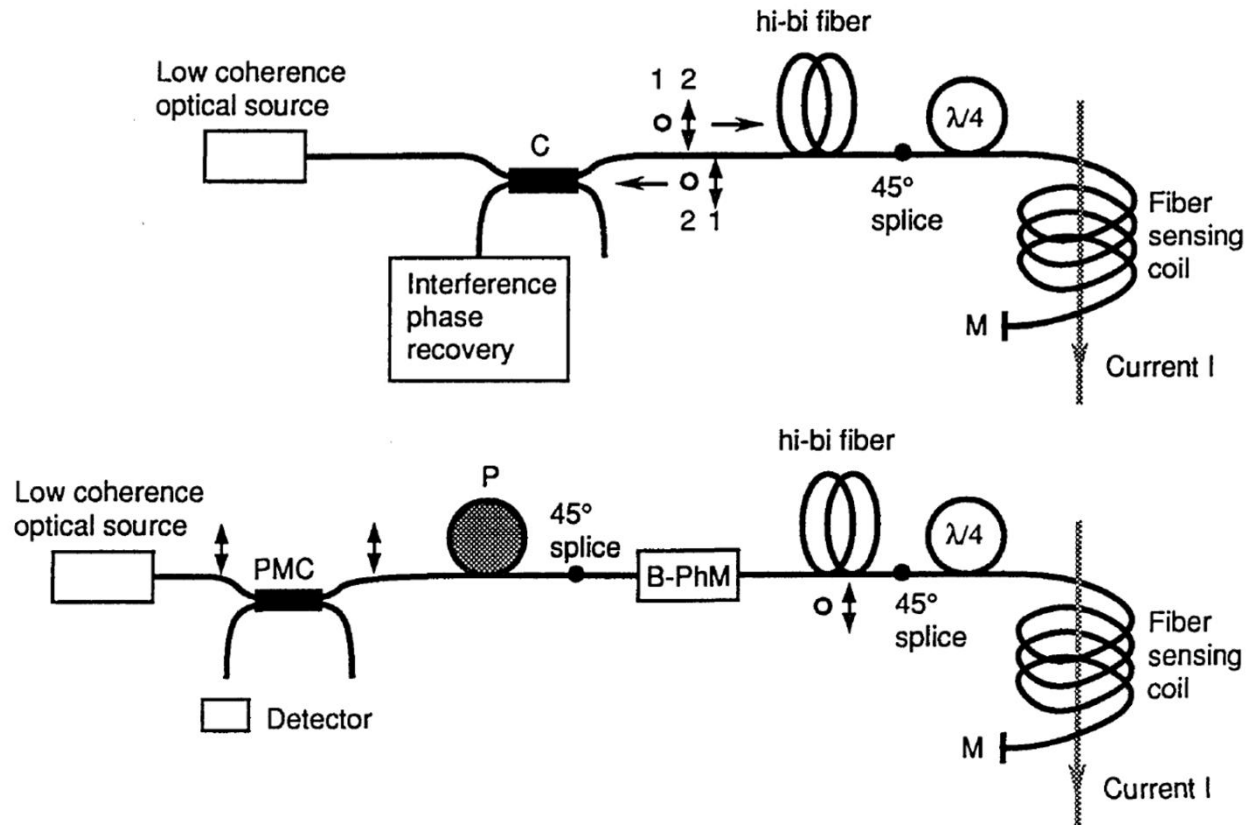
# Interferometric methods

- Using a laser, the setup becomes an interferometer of the Sagnac type
- Fiber optic gyroscope
- Extremely sensitive...
- ...to all changes in the fiber: length, temperature, vibration, etc.



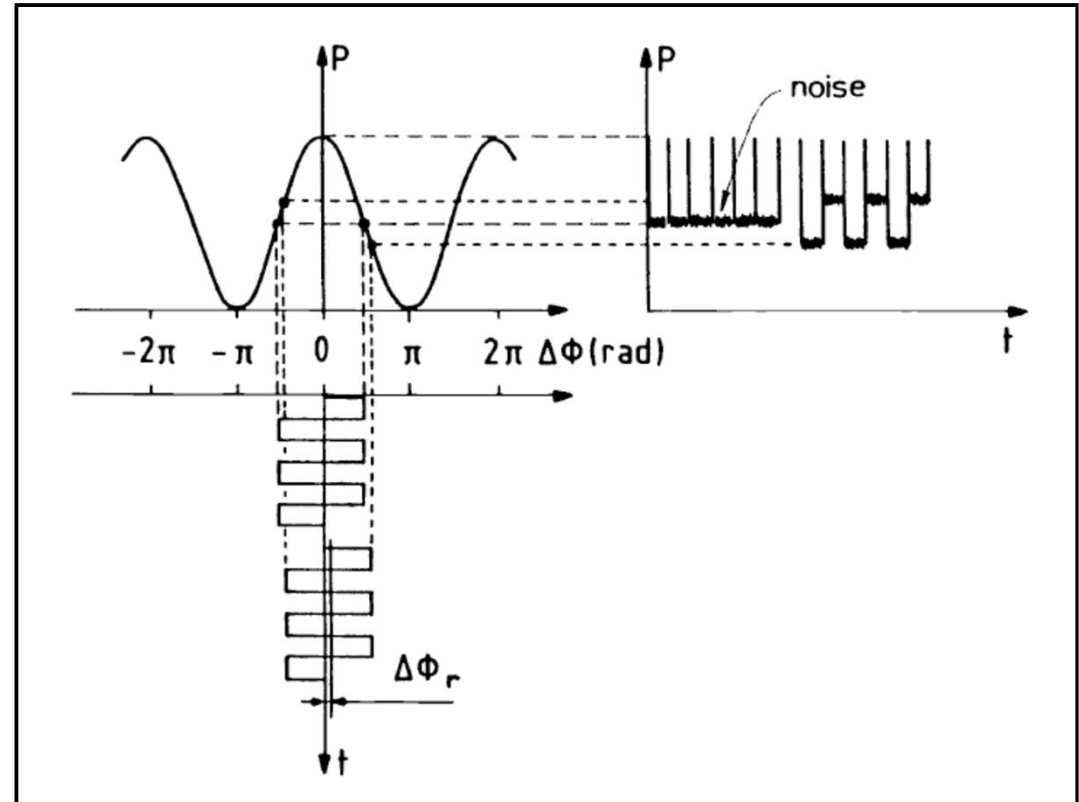
# Phase modulation

- Use a broadband source to avoid interferometric effects – superluminescent diode
- Frosio and Dändliker (1994)
- Highly nonlinear response
- Introduction of a phase modulator
- The detected intensity is proportional to an expression which can be expressed as the sum of Bessel functions



# Square-wave modulation

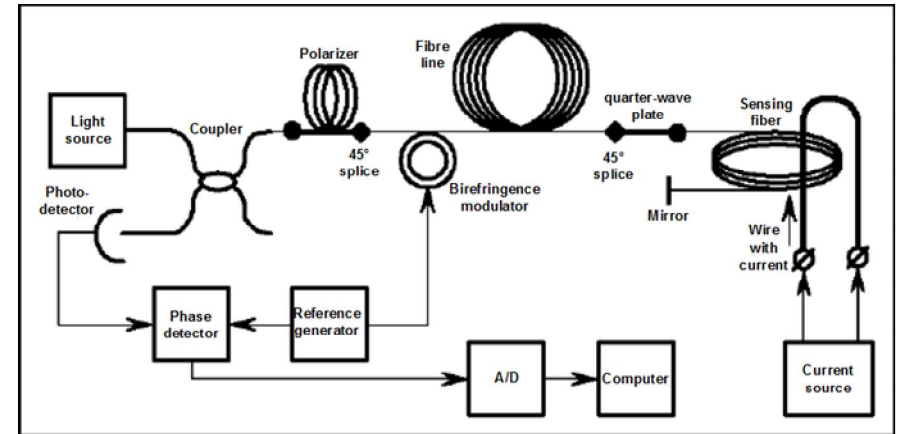
- Sinewave response is nonlinear and can suffer from wrap-around
- H. C. Lefevre *et al.* (1990)
- Bias to linear regime
- PID regulation to keep the operating point





# Profotech setup

- Use Jones-matrices to describe each component
- Polarization state is determined by the relative amplitude and relative phase
- Reciprocity means many errors cancel out
- Resulting power on the detector



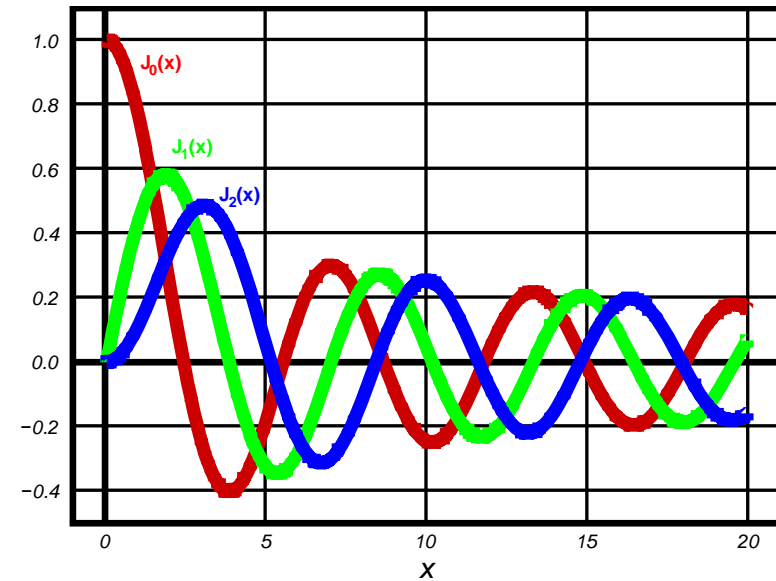
$$\begin{aligned}
 P(t) = & \frac{P_0}{2} + \frac{P_0}{2} J_0(4A_m \sin(\omega_0 \Delta t)) [\text{Re}^2(u) - \text{Re}^2(v)] \\
 & + \frac{P_0}{2} J_0(4A_m \cos(\omega_0 \Delta t)) [\text{Im}^2(u) - \text{Im}^2(v)] \\
 & + P_0 J_1(4A_m \sin(\omega_0 \Delta t)) \sin(\omega_0 t) 2 \text{Re}(u) \text{Re}(v) \\
 & - P_0 J_1(4A_m \cos(\omega_0 \Delta t)) \cos(\omega_0 t) 2 \text{Im}(u) \text{Im}(v) \\
 & + P_0 J_2(4A_m \sin(\omega_0 \Delta t)) \cos(2\omega_0 t) [\text{Re}^2(u) - \text{Re}^2(v)] \\
 & - P_0 J_2(4A_m \cos(\omega_0 \Delta t)) \cos(2\omega_0 t) [\text{Im}^2(u) - \text{Im}^2(v)]
 \end{aligned}$$

## FOCS setup

- Bessel functions result from Fourier-expansion
- Two parameters can be chosen to linearize the response –  $A_m$  and  $\omega_0$

$$J_1(4A_m \sin(\omega_0 \Delta t)) = J_2(4A_m \sin(\omega_0 \Delta t))$$

$$J_2(4A_m \cos(\omega_0 \Delta t)) = 0$$



$$\begin{aligned}
 P(t) = & \frac{P_0}{2} + \frac{P_0}{2} J_0(4A_m \sin(\omega_0 \Delta t)) [\text{Re}^2(u) - \text{Re}^2(v)] \\
 & + \frac{P_0}{2} J_0(4A_m \cos(\omega_0 \Delta t)) [\text{Im}^2(u) - \text{Im}^2(v)] \\
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 & - P_0 J_2(4A_m \cos(\omega_0 \Delta t)) \cos(2\omega_0 t) [\text{Im}^2(u) - \text{Im}^2(v)]
 \end{aligned}$$



## FOCS setup

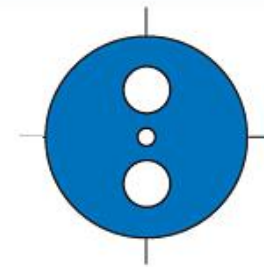
- Detect the signal at  $\omega_0$  and  $2\omega_0$  using a lock-in amplifier
- The ratio is proportional to the polarization change  $q_f$ , which is proportional to the current  $I(t)$
- $\tan \theta_f \propto \frac{P_{\cos(2\omega_0 t)}(t)}{P_{\cos(\omega_0 t)}(t)}$ , where  $\theta_f = \int \mathbf{B} \cdot d\mathbf{l} = \mu_0 \int N I(t)$

# Fiber properties

- Short wavelength – increases the Verdet constant
- Possibly doping – increases the Verdet constant
- Fiber has bending-induced birefringence which may mask the effect – use spun fiber
- Polarization maintaining (PM) fiber – since we are measuring polarization



Bow-tie type



Panda type



# THANK YOU!

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